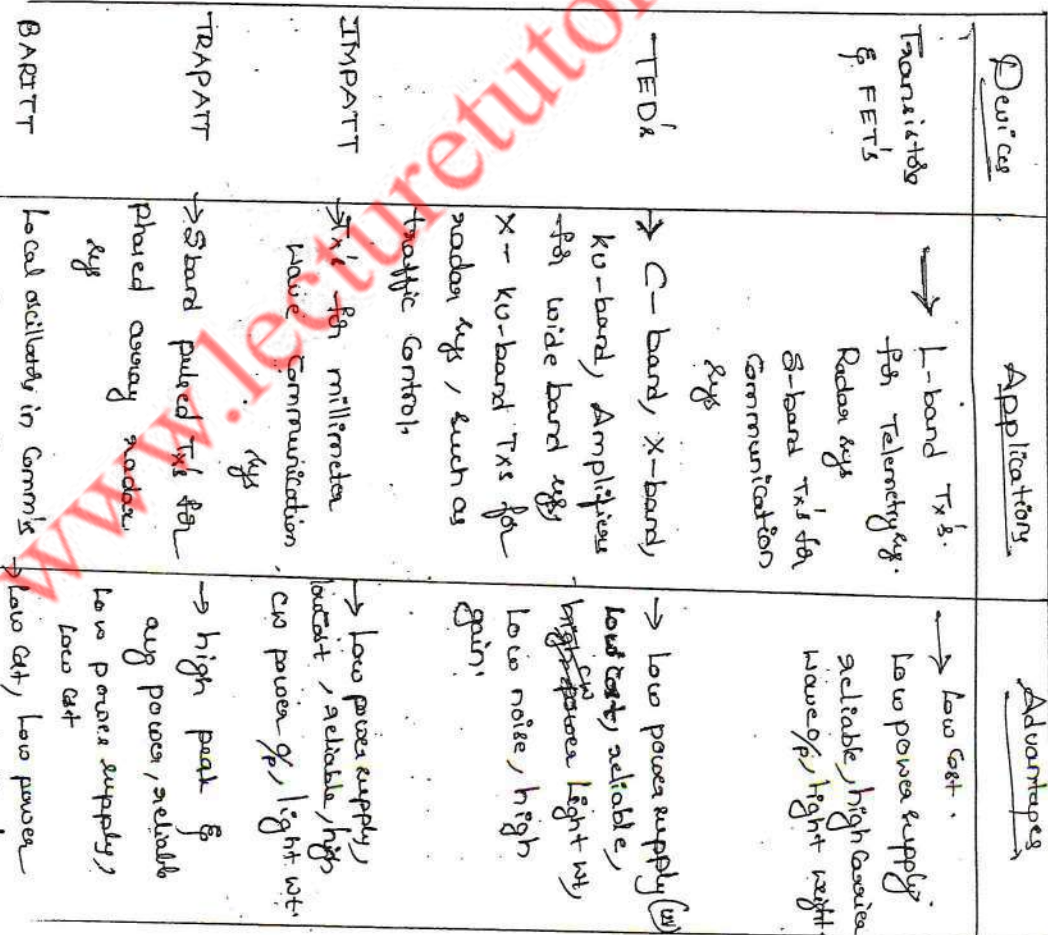


⑤

microwave devices, of two terminal & three terminal type.

Two terminal $\rightarrow$ TEDs, Avalanche transit time devices.

PMIGs have solid state devices



(2)

Applications of Solid State devices:

- 1) Amplification
2) Power conversion
3) up conversion
4) modulation
5) switching
- a) power generation
b) phase shifting

Ques: Explain Gunn effect using two valley theory and draw I-V char of Gunn diode.

Ans: TEDs are bulk devices having no junction (pn) gates.

* These are fabricated from compound semiconductors such as GaAs, InP (Indium phosphide) and CdTe (Cadmium telluride) instead of Si & Ge as that of normal transistors.

* TEDs operate with hot electrons whose energy is very much greater than thermal energy (≈ 0.025 eV at room temp), whereas transistors operate with warm electrons whose energy at room temp.

* TEDs exhibit negative resistance char. i.e., over a range of frequencies, the impedance is negative.

* Negative resistance char means "I & V" are out of phase by 180° , and a power of $(-I^2R)$ is generated.

The -ve resistance devices exhibit generated power. Active devices

* The resistance has "I" & "V" in phase and a power (I^2R) is dissipated/absorbed (passive elements).

* Example of TEDs is Gunn diode, LSA diode,

In TEDs we observe bulk effect of when potential, under the strong electric field, we observe a reduction of drift velocity, and thereby

ing electric field above V_{th} , the electrons shift from high mobility state to low mobility state.

This phenomena of transferring of electrons is exhibited in TEDs (Gunn diode).

Gunn diode:

Gunn diode are named after J.B. Gunn (1963) who discovered the current fluctuations of when current passing through the $Ni_{1-x}Ga_xAs$, when applied voltage applied exceed a critical value ($\approx 4 \text{ kV/cm}$).

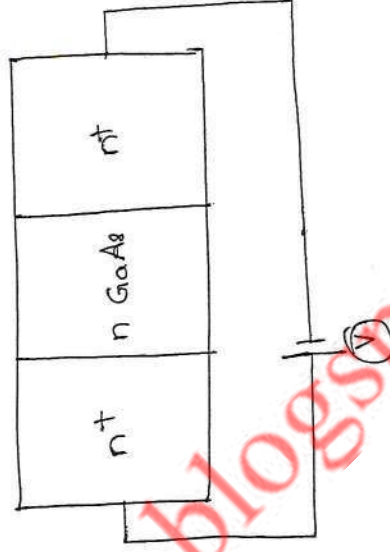
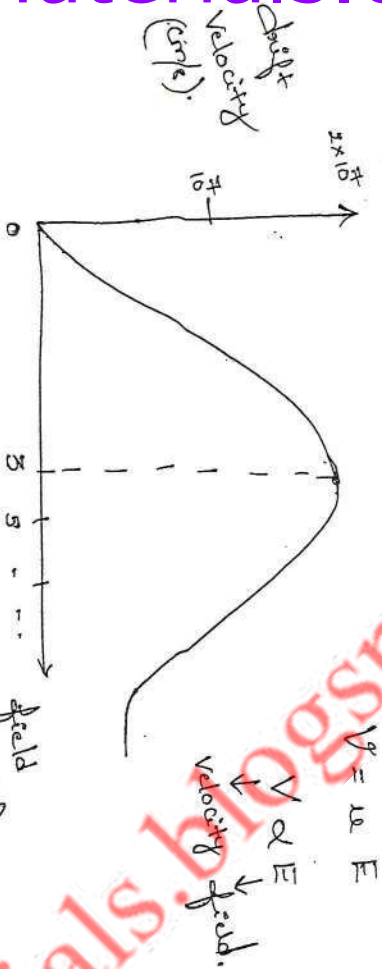


Fig: Gunn diode structure & char.

(3)

Gunn effect can be explained observed the GaAs drift velocity is linearly increased from zero to maximum, when electric field is varied from zero to a threshold value (3000 V/cm), After the E_{th} , the velocity is decreased and diode exhibits -ve resistance.



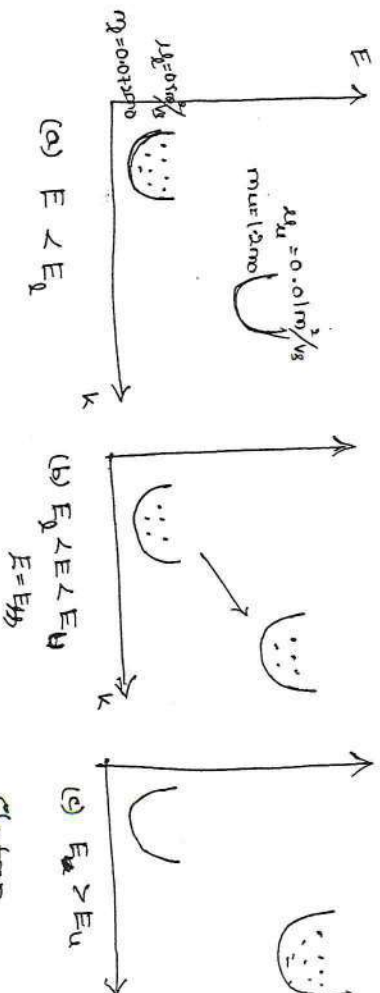
The E_{th} may vary with length & type of material

$$\therefore E_{th} = \frac{V}{L}$$

The Gunn effect is easily explained by using the two valley theory of Ridley Watkins-Hilsum (RWH) Theory (3) Transferred electron mechanism.

Principle: RWH / Two valley theory:

In this theory we consider two valley in conduction band lower valley, upper valley.



under electron equilibrium conditions, electron density is constant.

When an electric field is applied, then the mobility, density of e^- vary.

* When applied field (E) is lower than field of lower valley ($E < E_l$), there is no transfer of e^- from lower to upper valley.

* When $E_l < E < E_u$, the electrons will begin to transfer to the upper valley.

* When $E > E_u$, then all the electrons will transfer to upper valley.

(14)

Let mobility of $\bar{e}$ s in lower valley is $\mu_l = 0.5 \text{ m}^2/\text{Vs}$, mass of $\bar{e}$ is $m_l = 0.07 m_0$
In upper valley $\mu_u = 0.01 \text{ m}^2/\text{Vs}$, mass of $\bar{e}$ is $m_u = 1.2 m_0$.

Let n_l, n_u be the electron density of lower and upper valleys.

- * ie When $\bar{e}$ s are in L valley, mobility is high, mass of $\bar{e}$ is low, hence current density J is high.
- * When a field is applied which is equal $E_{th} \approx 3 \text{ kV/cm}$ at which $\bar{e}$ s complete transfer to upper valley.
- * In U-Valley mobility (μ_u) is low, mass of $\bar{e}$ is high, hence current density J is decreased.

$$J = \sigma E \quad \sigma = (\mu_l n_l + \mu_u n_u)$$

$$\Rightarrow J = (\mu_l n_l + \mu_u n_u) E$$

When $E > E_{th} \Rightarrow J = \mu_l n_l E$

$$n = n_l + n_u$$

= electron density
 $e =$ electron charge.

Modes of operation:

Depending on the material parameters & operating conditions, the Gunn diode operates in four frequency modes

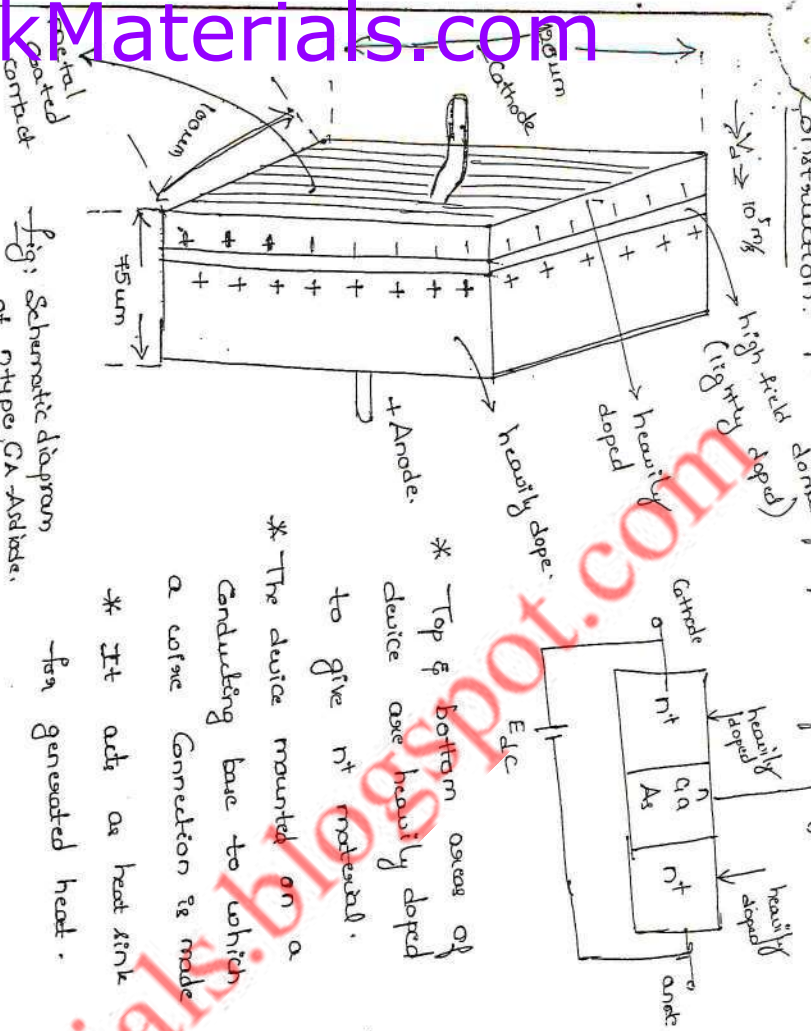
(a)

Q: Determine Conductivity of an n-type GaAs Gunn diode
electron density $n = 10^{18} \text{ cm}^{-3}$, n at lower valley $n_l = 10^{10} \text{ cm}^{-3}$
 n at upper valley $= 10^{18} \text{ cm}^{-3}$, temp $= T = 300^\circ \text{K}$

$$\begin{aligned} \sigma &= e (\mu_l n_l + \mu_u n_u) \\ &= 1.6 \times 10^{-19} (0.5 \times 10^{10} + \end{aligned}$$

$$e = 1.6 \times 10^{-19}$$

Explain the construction and operation of a Gunn diode.



* Top & bottom areas of device are heavily doped to give n⁺ material.

* The device mounted on a conducting base to which a wire connection is made

* It acts as heat sink for generated heat.

* The connection to other terminal of diode is made via field connection deposited on to the top surface.

The center area is active region, hence all the voltage placed across device appears across this region.

Explain about domain formation using relevant diagram in Gunn diode.

Operation of Gunn diode: (High field domain formation)

* When voltage is applied across GaAs crystal

Exceeds E_{th} , e^- are transferred from lower

energy band (high mobility) to higher energy (low mobility)

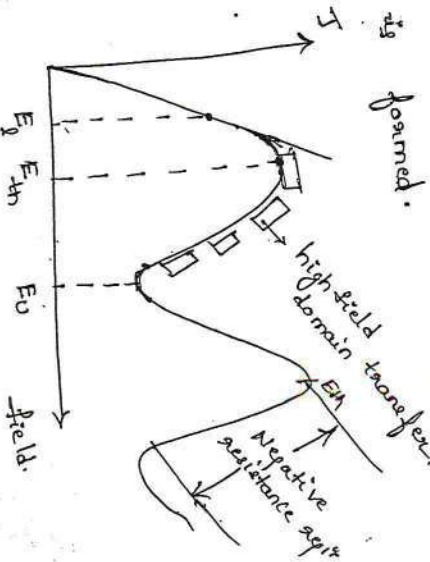
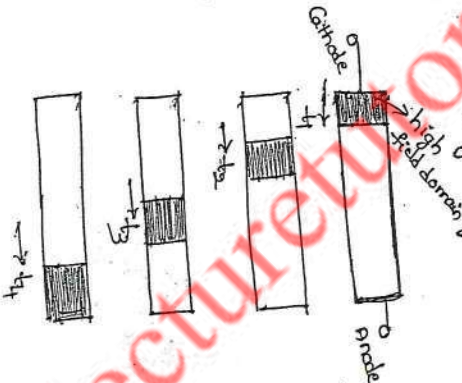
In which these electrons bunch together to form domain near the cathode.

* Due to this the electric field across domain rises but it is below E_{th} across the crystal to prevent further domains.

* But upper band is low mobile, the velocity of the e^- is decreased, hence current present in domain also ↓.

* Hence the high field domain is travelled in to the end contact.

* After reaching end, due to change in voltage, current again returns to higher level, again a high field domain is formed.



Each domain results a pulse of current at the %
These current fluctuations occurs at RF freq to C
Produce a % signal with a period equal to Transit
time.

Transit time (t_p):

Time taken by the high field domain to
travel from Cathode to Anode is called
Transit time.

Oscillation frequency:

$$f_o = \frac{1}{T_o}$$

$T_o = \text{oscillation frequency time period.}$



Basic modes of operation:

According to material parameters & operating
Conditions, Gunn diodes takes four modes.

① Gunn oscillator mode:

$$\text{Operating freq } (f_o) \times \text{Length } (L) = 10^7 \text{ cm/sec}$$

$$\text{Doping } (n_0) \times \text{Length } (L) \geq 10^2 / \text{cm}^2$$

(n+)

This is unstable mode. High freq oscillations
achieved when device operated with high-Q
cavity resonator. The diode is mounted at center of a
broad wall. The diode is mounted inside a cavity formed
by shorted termination at one end by an iris at
other inside.
 $f_o = V_d / L$

② Stable Amplification mode: This mode is defined in
region where.

$$V_d = f_o \times L \geq 10^7 \text{ cm/sec}$$

$$n_0 \times L \geq 10^{10} - 10^{12} / \text{cm}^2$$

③ LSA oscillation mode:

$$V_d = f_o \times L \geq 2 \times 10^7 \text{ cm/sec}$$

$$f_o = \frac{1}{T_o} = \frac{1}{\text{oscillation period.}}$$

In this mode Gunn diode placed in resonator which
is tuned to a freq f_o .

④ Bias Circuit oscillation mode:

$f_o \times L = \text{Very small. The device is biased}$
at threshold, f_o can be obtain in range of k-loc

Gunn oscillation mode:

Refer Pg 15

The input diode connects

It operates at reverse bias.

→ Impact ionization happens in lattice/
Cause a force e^- to hit an atom

Any diode exhibits +ve resistance
Forward bias action. The reverse char
and release an
Char in

in the Reverse Direction.

in the reverse bias. The Zener diodes are used as amplifiers, oscillators.

3-100 GHz

→ They operate at high freq
→ Adv: High power capability.

Adv: High power capability.

Adv: High power
disadv: high level noise due to awareness transfer

class

Impact diode utilising avalanche breakdown combine with transistors of charge carriers to enable it to provide a -ve resistance region

Characteristics:

In forward direction it will conduct, after it reaches conduction point.

In reverse direction, it will block current

How even at certain voltage the diode break down
and I will flow in reverse direction.

$p^+ =$ heavily doped

Proposition

heavily doped section.

In Reverse bias,

the holes in Pargion,

the e^- in region are attracted to the edge of the diode, leaving the minority carriers

After the in voltage the velocity of carriers

Yes if they knock the capital structure from

which e^- & holes are released. Again the majority

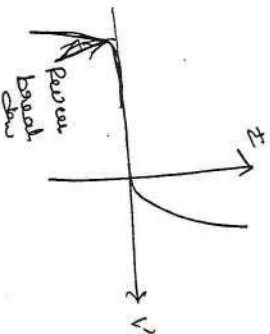
Coaxing are attracted to walls, and so minority.

causing them. Then for the movement of minority.

Carriers the current paths are obscured.

$\rightarrow$ The $\uparrow$ of e^- & holes due to γ breakdown is

Called as Impact formation.



⑧

In terms of operation Impatt diode has two regions

① Avalanche / Injection region

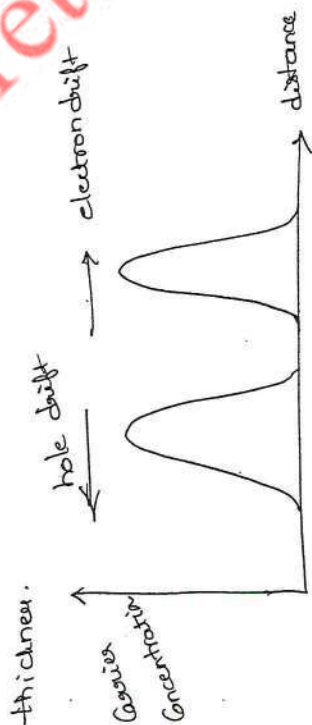
② Drift Region.

Injection Region:

It creates the Carriers which may be holes/e⁻s.

Drift Region:

Carriers move across the drift taking $\frac{L}{v}$ is, where L is a certain amount of time dependent upon its thickness.



Charge Carrier movement within Impatt diode.

* Majorly the drift effect is not seen for DC, but for AC we can see the drift.

* When an AC signal applied the Carrier peaks are found to be 180° out of phase with the Voltage.

* This is due to two delays which occur in device.

- ① Injection delay
- ② Transit time delay.

i.e Time taken for Carriers migrate & drift across the device is nothing but delay b/w of Current peak production.

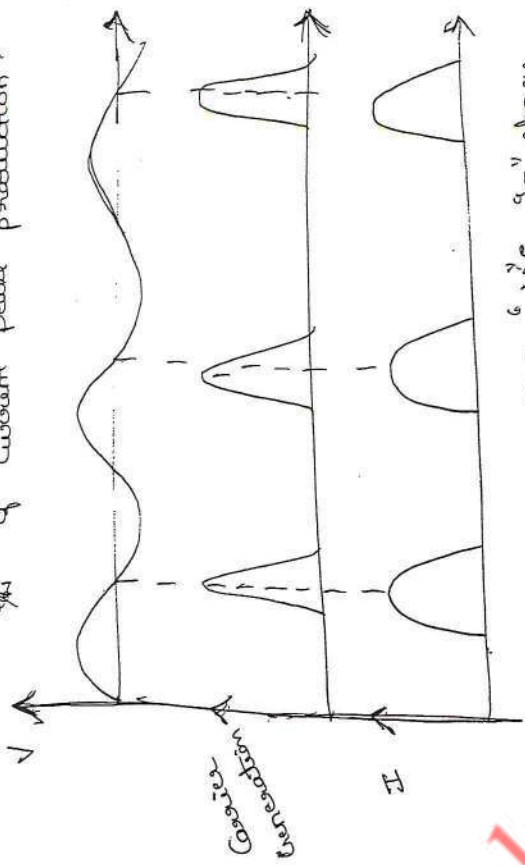


fig: Impatt diode "V & I" char

* electric field rises, no of Carriers rises, when field reaches max also, the Carriers still continue to grow as a result of no of Carriers already in existence.

* As a result of this there is a phase lag of 90° b/w I & V. This is known as Injection phase delay

* when e⁻s move across N⁺ region an External Current is seen after a delay of another 90°.

By connecting a tuned circuit along with a Voltage (break down) oscillation will occur with a resonant frequency.

$$\text{Resonant frequency } (f_0) = \frac{V_d}{2L}$$

V_d = drift velocity
 L = length of drift space region.

Disadvantages:

- (1) It is very noisy because avalanche process is noisy process.
- (2) The devices based around Ga-As are better than Si.
- (3) Tuning range is not good.

Performance characteristics:

$$\eta = \frac{P_{ac}}{P_{dc}} = \frac{V_a I_a}{V_d I_d}$$

P_{ac} = ac power
 P_{dc} = dc power
 V_a, I_a = AC Voltage / current
 V_d, I_d = DC Voltage / current

$$\eta \approx 30\% \text{ (In practical)}$$

15% for Si, 33% for Ga-As

frequency: 1-300 GHz

max % power for single diodes 5W in X band
0.5W at 300GHz

max % power for several diodes combined:
40W at X band.

pulsed power $\approx 4kW$.



Applications:

- 1) These are used as oscillators such as
 - (a) microwave generators
 - (b) modulated % oscillators
 - (c) Receiver local oscillators
- 2) These are suitable for -ve resistance amplification.
- 3) High Quality IMPATT diodes are used in
 - (a) Instrumentation systems
 - (b) police radar
 - (c) low power microwave

Q: An IMPATT diode has following parameters.

CARRIER drift velocity $V_d = 2 \times 10^6 \text{ cm/s}$

drift region length $L = 6 \mu\text{m}$

Max operating voltage $V_{o \text{ max}} = 100V$

Max operating current $I_{o \text{ max}} = 800 \text{ mA}$

$$\eta = 15\%$$

Breakdown voltage $V_{bd} = 90V$

Find

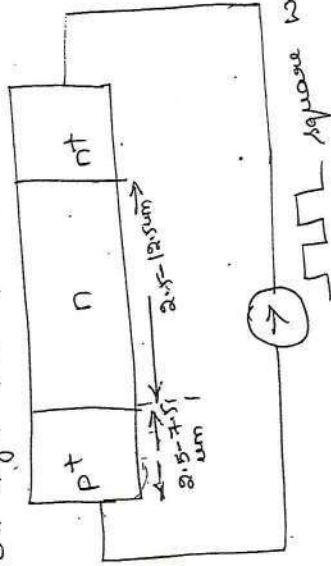
- (a) Max Carrier wave % power in watts
- (b) Resonant freq in GHz.

sol: $\eta = \frac{P_{ac}}{P_{dc}} \Rightarrow$

What are avalanche diodes - Explain schematic and operation of IMPATT diode. Also explain typical V-I characteristics of IMPATT diode.

Trapped diode: (trapped plasma time devices).

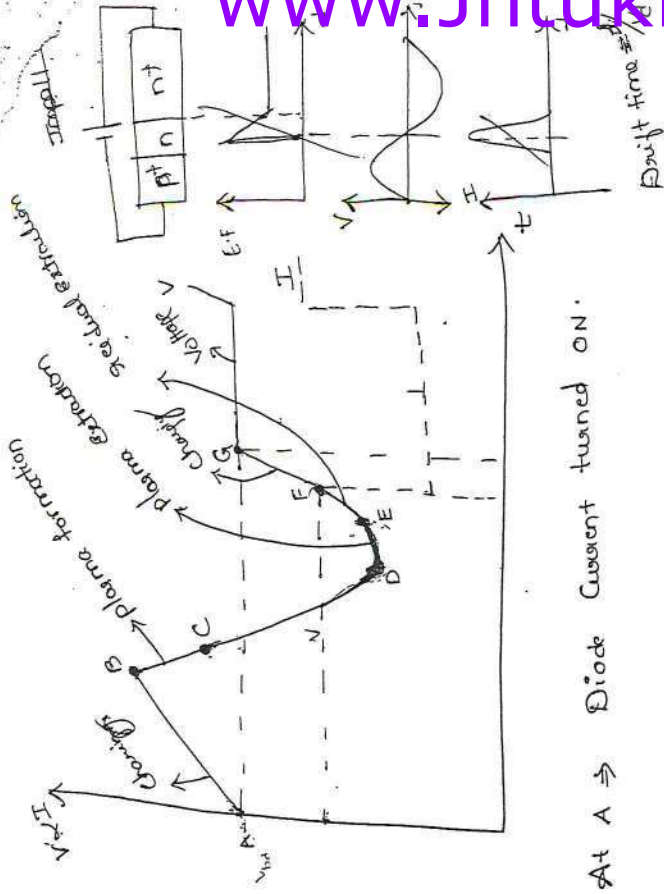
- * Trapatt diode is similar to that of the Impatt diode but it is advantageous in a way γ is up to 20-60%
- * The construction of the device consists of p^+-n-n^+ layers, but the doping levels are $p^+ = 2.5$ to 7.5 cm^{-3} , $n = 2.5$ to 12.5 cm^{-3} depletion layer.
- * Manufactured from Ge, Si, GaAs, InP.
- * For high peak power we use n^+-p-p^+ structure.



The diameter of diode is 50um.

(a) Current pulse generator.

- * In trapatt diode, the mode does not depend on the Avalanche phase delay.
- * Because Avalanche multiplication is faster than that of the drift velocity of the carriers by a factor "3".
- Hence no delay for Avalanche breakdown.
- * To prevent burning of diode, a current bias source is used to maintain an avg current at safe limits.
- * The diode current contributed by e^- move from p^+ to drift space region and then to n^+ .



At A $\Rightarrow$ Diode Current turned ON.

A high field avalanche zone propagates through diode and fills depletion layer with a dense plasma of e^-/h^+ become trapped in low field region behind zone.

* A typical 'V' wave form for Trapatt diode operates with square wave current is assumed to be as below.

At A: Electric field is uniform through out the sample, i_f may be large but less than of avalanche BD.

Current density expressed as $J =$

$\therefore$ At A $\Rightarrow$ diode is turned ON.

Hence at 'A' the diode starting to charge like a linear Capacitance, hence the electric field increases above the breakdown voltage.

→ At 'B', when a sufficient no. of carriers are generated, the internal current exceeds the external current.

Hence the voltage field is decreased through out the depletion region. Hence voltage decreased to "E" from "B".

→ At "C", we observe electric field voltage is still more than sufficient for avalanche to continue, hence still dense plasma of e^- & holes is created, hence internal current still increases, result in decrease of voltage further to "D".

Due to heavy release, some of e^- , holes may drift out of the ends of the depletion region hence voltage decreases to "D".

A long time is required to remove the plasma because plasma charge is very large compared to charge per unit area in external current.

$$i_i = \frac{qV_p}{t} \quad i_e = \frac{qV}{t}$$

$$i_i > i_e$$

Hence in order to reduce it, the plasma charge should be removed.

Hence after removal of plasma i_i will be reduced, the voltage will be $\uparrow$ ed from D to "E".

* After removal of plasma a residual charge is observed, where a residual charge of e^- is on one side, residual charge of holes on other side.

* As the residual charge is removed, voltage $\uparrow$ es from "E" to "F".
ie, At "F" all the charge that was generated will be removed.

* From "F" the diode charges up ^{again} like a fixed capacitor.

Avalance Zone velocity $V_z = \frac{dx}{dt} = \frac{x}{t}$

$t =$ Current density
 $q =$ electron charge
 $N_A =$ doping concentration.

Q: A Trapath diode has $N_A = 2 \times 10^{15} \text{ cm}^{-3}$ & $\tau = 20 \text{ ns}$. Calculate V_z .

$$V_z = \frac{x}{t} = \frac{20 \times 10^{-9}}{1.6 \times 10^{-9} \times 2 \times 10^{15}} = 6.25 \times 10^4 \text{ cm/s}$$

Trapath diode

Specifications / Chars:

- 1) CN power = 1-3W f_N 8GHz to 0.5GHz
- 2) pulsed power = 1.2kW at 1.1GHz
- 3) operating Voltage = 60-150V
- 4) $\eta =$ up to 40%.

12) Noise figure > 50db

13) frequency = 3-50GHz

Limitations

- * Sensitive to harmonics
- * More noisy due to avalanche process

Applications

- 1) used in low power doppler radar
- 2) Local oscillators for radar
- 3) radio altimeter
- 4) MW beacon landing sys.
- 5) phased array Radar.

Q: A Impatt diode has length L (drift velocity) of 2um.

find (a) drift time of carrier (b) operating freq. for



$$V_d = 2 \times 10^5 \text{ m/sec}$$

$$f_0 = \frac{1}{2\tau} = \frac{V_d}{2L}$$

$$\tau = \frac{L}{V_d} = \frac{2 \times 10^{-6}}{2 \times 10^5} = 2 \times 10^{-11} \text{ sec}$$

$$f_0 = \frac{1}{2\tau} = \frac{1}{2 \times 2 \times 10^{-11}} = \frac{1}{4 \times 10^{-11}} = 2.5 \times 10^{10} \text{ Hz} = 25 \text{ GHz}$$

$$\tau = \frac{L}{V_d}$$

$$\tau_1 + \tau_2 = T_0$$

Q: An Impatt diode has following parameters.

$V_d = 2 \times 10^5 \text{ cm/s}$ / drift length $L = 6 \text{ um}$,

drift velocity

max operating voltage $V_{\text{max}} = 100 \text{ V}$, max operating current $I_{\text{max}} = 200 \text{ mA}$

Efficiency $\eta = 15\%$, breakdown voltage $V_{\text{bd}} = 90 \text{ V}$.

find (a) Max carrier % power in watts.

(b) The resonant freq. f_0 .

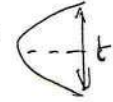
Sol:

$$\eta = \frac{P_{\text{ac}}}{P_{\text{dc}}} \quad P_{\text{ac}} = \eta P_{\text{dc}} = 0.15 \times 20 = 3 \text{ W}$$

$$P_{\text{dc}} = V_d \times I_d = 100 \times 200 \times 10^{-3} = 20 \text{ W}$$

$$f_0 = \frac{1}{2\tau} = \frac{1}{2} \cdot \frac{V_d}{L} = \frac{2 \times 10^5}{2 \times 6 \times 10^{-6}} = 1.67 \times 10^{10} \text{ Hz}$$

$$\eta = \frac{P_{\text{ac}}}{P_{\text{dc}}} = 0.15$$



$$V_d = fL$$

$$f = \frac{V_d}{L}$$

$$\tau = \frac{L}{V_d}$$

$$\tau = \frac{L}{V_d}$$

Q: A Ku band IMPATT diode has

pulse operating voltage of 100 V &

current of 0.9 A, η is of 10%. Calculate.

1) % power 2) duty cycle of pulse width of 0.01 ns

& freq is 16 GHz

(a) % power $P_{\text{ac}} = \eta P_{\text{dc}}$

$$= \frac{10}{100} \times (V_d \times I_d) = 0.1 \times 100 \times 0.9 = 9 \text{ W}$$

$$\text{Duty cycle} = \frac{\text{pulse duration}}{\text{pulse repetition period}} = \frac{\tau}{T}$$

$$= \frac{0.01 \times 10^{-9}}{T} = 0.01 \times 10^{-9} \times 16 \times 10^9 = 0.16 = 16\%$$

$$f = \frac{1}{T}$$

In a Gunn diode active length of 800 μm ,
drift velocity of $e^- = 3 \times 10^6 \text{ cm/s}$. Calculate natural freq.

§ Critical voltage of diode.

Sol: $f = \frac{V_d}{L} = \frac{2 \times 10^7}{80 \times 10^{-6}} \times 1 \times 10^{-12} = 1000 \text{ GHz}$

Critical voltage $V = 1 \times \text{critical field}$

$= 20 \times 10^{-6} \times 3.3 \times 10^8 \text{ V} = 6.6 \text{ V}$

$V_{d \text{ field } V}$

Kodlapratheem3@gmail.com

TRAPATT diode :-

Specifications:-

- 1) CW power : 1-3W b/w 8GHz to 0.5GHz
- 2) Pulsed power : 1.2 KW at 1.1GHz
- 3) operating voltage : 60-150V
- 4) η : 15 to 40%
- 5) Noise figure > 30dB
- 6) Frequency : 3 to 50 GHz.

Limitations:-

- These diodes are very sensitive to harmonics.
- more noisy because of avalanche.

Applications:-

- 1) used in low power doppler radars
- 2) local oscillator for radars
- 3) radio altimeter
- 4) phased array radar
- 5) MJO beacon landing system etc.

41, 5, 11, 12, 15, 16, 17, 18, 23, 24, 25, 28, 29, 30, 32, 33, 34, 36, 37, 40, 42, 43, 45, 46, 50, 51, 52, 54, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100

31, 7, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100



TRAPATT diode

TRAPATT diode

TRAPATT diode

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TRAPATT diode

The avalanche zone velocity,

$$v_z = \frac{dq}{dt} = \frac{J}{qN_A}$$

where N_A = doping concentration.

The highest pulse power of 1.2 kW has been obtained at 1.1 GHz, and the highest efficiency 75% has been achieved at 0.6 GHz. The TRAPATT diode generally exhibits a higher noise figure than the IMPATT diode and the upper operating frequency appears to be practically limited to below the millimeter wave region.

5) A TRAPATT diode has the following parameters: doping concentration, $N_A = 2 \times 10^{15}/\text{cm}^3$ and current density, $J = 50 \text{ kA}/\text{cm}^2$. Calculate the avalanche zone velocity.

$$v_z = \frac{J}{qN_A}$$

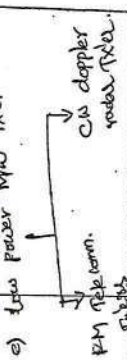
$$= \frac{50 \times 10^3}{1.6 \times 10^{19} \times 2 \times 10^{15}}$$

$$v_z = 6.25 \times 10^7 \text{ cm/s}$$

This means that the avalanche zone velocity is much higher than the scattering limited velocity.

Applications

- These are used as oscillators such as:
 - 1) MJO generators
 - 2) modulated oscillator
 - 3) reactor local oscillator
 - 4) low amp pumpers
- These diodes are also suitable for:
 - negative feedback amplification.
 - high quality TRAPATT diodes are used in:
 - a) Interference alarm
 - b) Police radar
 - c) Low power MJO mixer



IMPATT diode :-

Performance characteristics:-

- 1) η = 30% and 15% at 85% efficiency
- 2) Frequency : 1 to 300 GHz
- 3) Power : 0.5 W to 10 W
- 4) Noise figure : 40 dB at 10 GHz
- 5) Pulsed power : 4 kW

Advantages:-

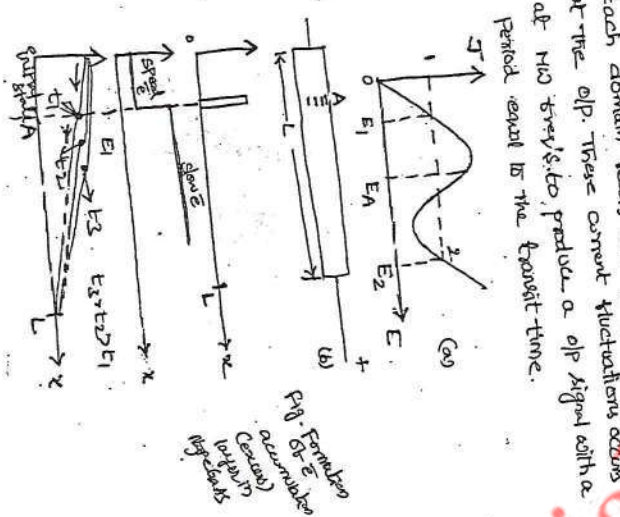
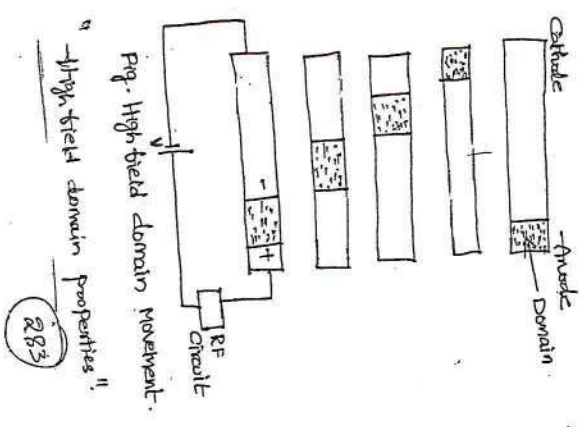
- 1) It is very noisy because avalanche is a noisy process.
- 2) Tuning range is not good.

13

High field domain formation :-

When the voltage applied across an n-type GaAs crystal exceeds a threshold level, electrons are transferred from the low energy, high mobility conduction band to a higher energy, low mobility sub-conduction band, where these heavier electrons bunch together to form an electric field dipole domain near the cathode. Since the applied voltage remains constant, the electric field across the domain is greater than the average field. The consequent $\pm$ field remains below the threshold level across rest of the crystal. This prevents the formation of further domains.

All the conduction band electrons drift across the crystal at the same velocity and the low mobility bunched electrons have reduced velocity. The current in the presence of domain also decreases. After the high field domain had travelled the end contact, the current returns to its higher level and high field domain is again formed.



Gunn diode modes

Basic modes of operation :- According to material parameters & operating conditions, Gunn diode can be used in four basic modes.

- 1) Gunn oscillator mode (Transit-time mode)
- 2) Stable amplification mode
- 3) LSA oscillation mode
- 4) Bias cut oscillation mode.

1) Gunn oscillator mode :-

Operating frequency $(f) \times \text{length } (L) \approx 10^7 \text{ cm/sec}$
 $f \times \text{length } (L) \times \text{length } (L) > 10^7 \text{ cm}^2/\text{sec}$
 In this mode the device is unstable because of the cyclic formation of either accumulation layer or high field domain. Higher oscillation frequency can be obtained when the device is operated with a high Q cavity resonator.

2) Stable amplification mode :-

$$f \times L = 10^7 \text{ cm/sec}$$

$$n \times L = 10^8 \text{ to } 10^{10} \text{ cm}^2$$

3) LSA oscillation mode :-

$f \times L > 2 \times 10^7 \text{ cm/sec}$
 LSA mode is the simplest mode of operation. In LSA mode, the Gunn diode is placed in a resonator which is tuned to an oscillation frequency of f_0 .

$$f_0 = \frac{1}{T_0} = \text{oscillation period}$$

In this mode the device can be biased to several times the threshold voltage. As the d.c. RF voltage increases, above the threshold voltage, the device remains in the negative resistance region. The oscillating frequency is determined by the external components only & not by transit time carrier time.

d.c. power = 400 mW to 600 mW in pulsed mode.

Limitations of LSA mode :-

- 1) It is very sensitive to load.
- 2) sensitive to operating temperature.
- 3) variation in doping concentration affects the stability.

Bias current excitation :-

$f \times L$ is very small.
 The device is biased at threshold.
 The oscillating frequency is obtained in the range of 1 kHz to 100 MHz.

Typical characteristics :-

- 1) d.c. power : 25 mW to 150 mW
- 2) pulsed power : 50 mW (5-12 GHz)
- 3) $\eta = 2\%$ to 12%

Applications :-

- 1)
- 2)

$$\eta = \frac{P_{out}}{P_{in}}$$

$$= \frac{f \cdot L}{P_{in}}$$

1) Transit-time domain mode ($f_L \approx 10^7$ cm/s):

When the electron drift velocity v_d is equal to the sustain velocity v_s , the high field domain is stable. In other words, the electron drift velocity is given by

$$v_d = v_s = f_L \approx 10^7 \text{ cm/s.}$$

Then the oscillation period is equal to the transit time - that is, $\tau_o = \tau_L$. This situation is shown in fig. The efficiency is below 10% because the current is collected only when the domain arrives at the anode.

2) Delay-domain mode ($10^6 \text{ cm/s} < f_L < 10^7 \text{ cm/s}$):

When the transit time is chosen so that the domain is collected while $E < E_{th}$ as shown in fig., a new domain

10

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Difference between low frequency measurement & microwave frequency measurement

- 1) At lower frequency's power is obtained by multiplication of measured voltage & current. At high frequency power is obtained directly.
 - 2) At low frequency circuit is consists of lumped elements (R, L, C) where as at high frequency consists of distributed elements, impedance of the circuit is measured.
 - 3) Ratio of maximum to minimum power is calculated at high frequencies instead of input & output power.
 - 4) Parameters at high frequency are power, frequency, phase (impedance, attenuation, SWR & quality factor).
- Draw the block schematic of a typical Microwave test bench and explain functionality of each component.
- Description of Microwave Bench :-

The general set-up for measurement of any parameter in microwave is normally done by a microwave bench. It has different blocks those are

- 1) Signal Generator
- 2) variable precision attenuator
- 3) variable Flap Attenuator
- 4) Frequency meter
- 5) Slotted line
- 6) crystal detector probe
- 7) Standing wave indicator.

LET US DISCUSS EACH OF THESE COMPONENTS

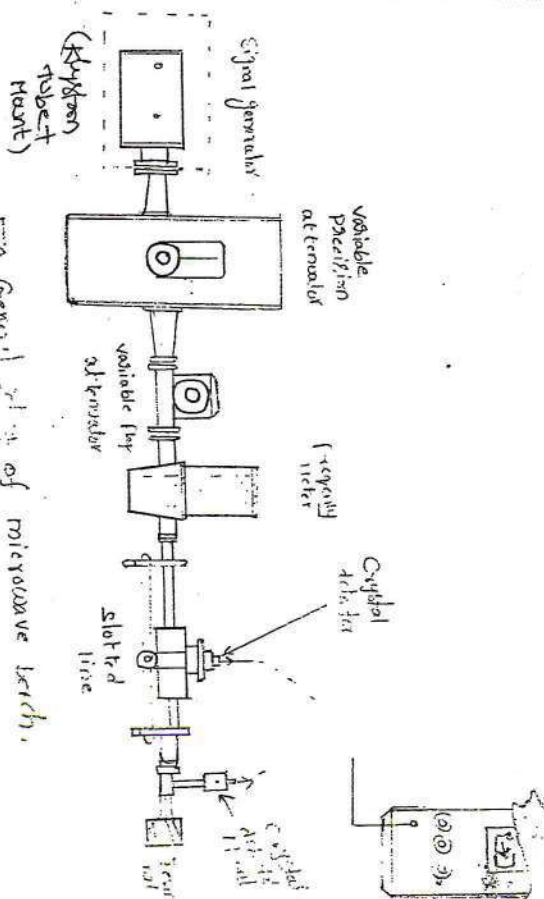


Fig. General set up of microwave bench.

Signal generator :-

It is a microwave source whose output is of the order of milliwatts. It could be Gurn diode oscillator, a backward wave oscillator or a klystron tube.

Klystron tube :- It makes use of velocity modulation to transfer continuous beam into microwave power. Electrons emitted from the cathode are accelerated and passes through the positive resonant cavity where negative feedback which retards and finally synchronizes the electrons and the electrons turn back through the resonator.

Klystron Power Supply :- It basically generates necessary frequency which is to be transmitted through the waveguide. It provides the beam voltage (anode) and repes voltage (cathode) to the klystron mount.

It provide 0 to 50dB attenuation above its insertion loss.

Variable flap Attenuation, - check its calibration against readings of the

Emergency meter :-

Frequency meter :-
It is used for direct reading of frequency that consists of single cylindrical cavity which can be adjusted to resonance and is slot couple to the waveguide. It helps to read the frequency of signal passing through the waveguide set-up. It is used at the intersection of horizontal and vertical rod lines.

Slotted Section :- In this section the waveguide is slotted by a gap and it is done as to adjust the amount of clock cycles at signal so that wavelength can be measured using vernier scale.

Crystal detector - is inserted in the E probe of the slotted in crystal detector probe at the end of the is contained in the crystal detector mount at the end of the modulated signal. waveguide run, is used to detect the

VSWR meter :-
- this indicator is basically a sensitive tuned voltmeter that provides direct reading of the SWR as its equivalent value in decibels.

Precautions :-

- 1) Components should be connected tightly for avoiding power leakage.

leakage.

2) Air cooling is required for rectifier thyriston oscillator.

- 2) Air cooling is required for
- 2) W/o power should not be measured directly as it effects the

vision (harmful to eyes).

① ②

Frequency Measurement :-

Micro wave frequency
mechanical Techniques.

Electronic Techniques :-

Electronic Techniques:-

These techniques generally more accurate and expensive. Frequency Counter or high frequency heterodyne systems can be used. Here the unknown frequency is compared with harmonics of a known lower frequency by use of a low frequency generator, a harmonic mixer.

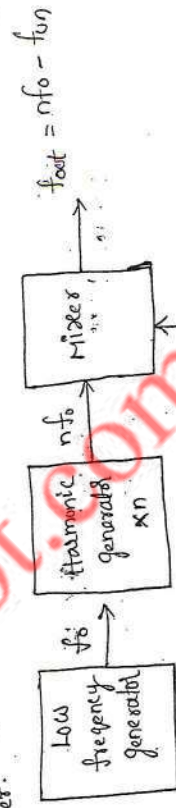


fig. Measurement of frequency - electronic method.

(P)

Measurement of Power:

The microwave power inside waveguide does not spread ^{very}

On position of measurement. For pair P

The technique used to measure power depends on, whether

Power is low/high.

The measurement techniques are of 3 types

① Measurement of low power (0.01mW - 10mW)

Bolometry

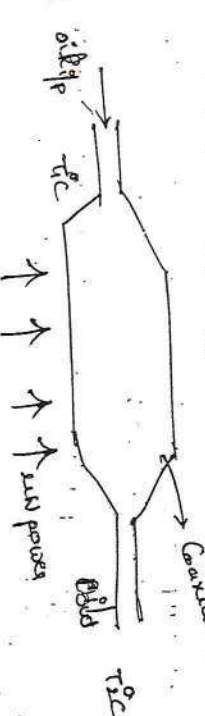
Medium pair (10mm-1m)

Calorimetric Technique

high power ($>10\text{ W}$)

—Calorimetric Watt meter.

Measurement of high porosity cable



Any power b/w 100 - 500W is considered to be high power. There are measured using calorimetric watt meter method.

It consists of a coaxial cable which is filled with circulating water / oil which is good absorber of microwave. The cable subjected to microwave power. The fluid after flowing through the lead experiences a temp rise due to ~~an~~ energy. The difference

T_g^c b/n T_g^c of known liquid before entering load and the after it emerges is a measure of points it absorbs.

$$R_{ik} = \frac{1}{n} \sum_{j=1}^n R_{ijk}$$

4.18

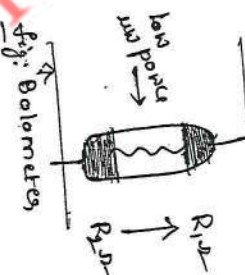
$\epsilon =$ specific gravity in g/cm^3

P = mean wind power in Watts
 R = rate of flow (cm^3/s)
 k = specific gravity heat in cal/g

Measurement of low power:

Bolometers / Thermocouples are devices whose resistance changes with applied power and are capable of measuring low power.

Yousef Gouda



Polymers simple temp.
Lohse Resistance versus temp.

They are of 2 types

② Thermistors



→ Banders have +ve temp coeff. R has with fac in temp.

Thermistors = -ve
RTD = +ve
PTC = +ve

→ ~~Butterfly~~ consists of a fine platinum wire mounted in cartridges

like an ordinary fue. transmission case. semi-conducta matches

→ Bolometer is a square law device, it produces current in

Proportional to applied power. Bolometer is mounted inside
... guide to measure operation resistance is $R_{1/2}$.

→ Now a lens with power applied, the same power is absorbed

by bolometer
charges to R₂.

change in R & microwave power

In the balanced bolometer bridge technique, the bolometer itself is made to be one of the arms of the bridge.

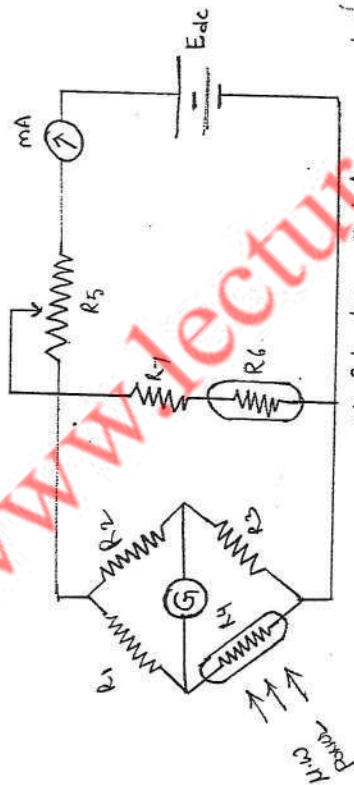


Fig. Bolometer method for measurement of power.

Initially, the bridge is balanced by adjusting R_5 , which varies the dc power applied to the bridge and the bolometer element is brought to a predetermined operating resistance before microwave power is applied. Let the voltage of the battery be E_1 at balance. The microwave power is now applied and this power gets dissipated in the bolometer. The bolometer heats up and it changes its resistance. Therefore the bridge becomes unbalanced. The applied dc power is changed to E_2 to get back the balance and the change in dc battery voltage ($E_1 - E_2$) will be proportional to the microwave power. Alternatively the detector G can be directly calibrated in terms of microwave power so that when the bridge is unbalanced, the detected power sends the microwave power directly.

Errors since bolometers are temperature sensitive, some form of temperature compensation has to be used to avoid errors. By R_6 and R_7 resistors this can be achieved.

Attenuation Measurement :-

Microwave components and devices almost always provide some degree of attenuation. Attenuation is the ratio of input power to the output power and is normally expressed as in decibels.

$$\text{i.e. Attenuation (in dB's)} = 10 \log \frac{P_{in}}{P_{out}}$$

where P_{in} = input power and

P_{out} = output power.

The amount of attenuation can be measured by two methods.

- power ratio method
- RP substitution method.

power Ratio method :-

This method involves measuring the input power and output power with and without the device whose attenuation is to be measured as shown in setup 1 and setup 2. The powers are measured in terms of P_1 and P_2 . The ratio of powers P_1/P_2 expressed in decibels gives the attenuation.

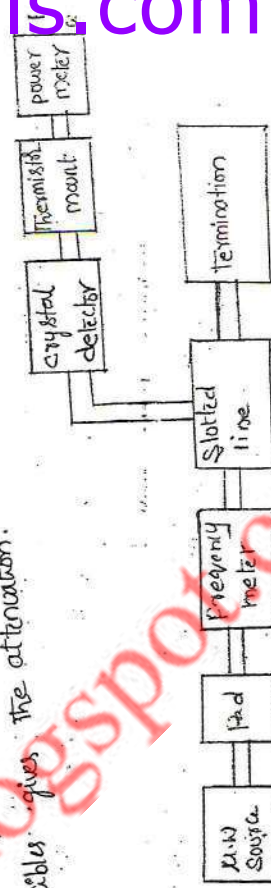


Fig. Setup 1, power ratio method.

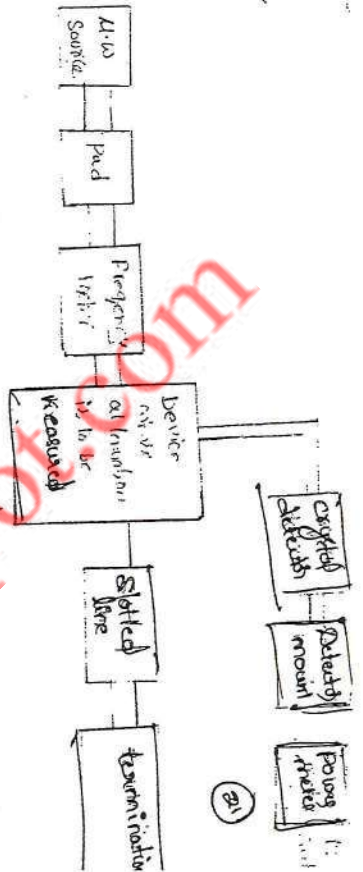


Fig. Setup2, Power ratio method

The drawback of this method is that the attenuation measured correspond to two power positions on the power meter with a square law crystal detector characteristics. Due to nonlinear characteristics the two powers measured and the attenuation calculated will not be accurately particularly if the attenuation of the network is large and if the input power is low.

RF Substitution method:-

This method overcomes the drawback of power ratio method since there we measure attenuation at single power position. The method consists of measuring the output power say 'P' by including the network whose attenuation is to be measured in setup1 as shown in fig.

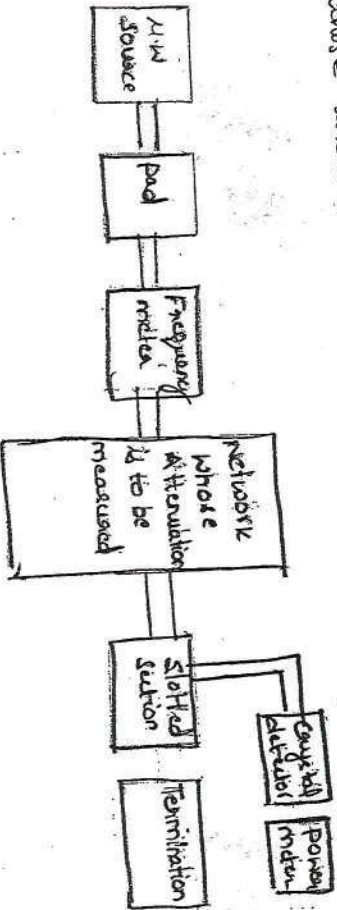


Fig. Setup1, RF Substitution method

In Setup2, this network is replaced by a variable attenuator which can be adjusted to obtain the same power 'P' as measured in Setup1. Under this condition the attenuation read on the precision attenuator could give attenuation of the network directly.

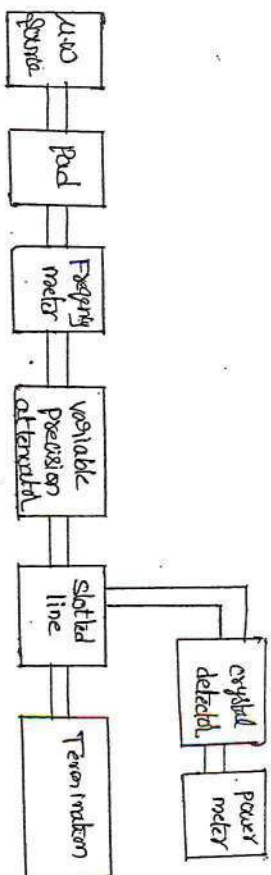
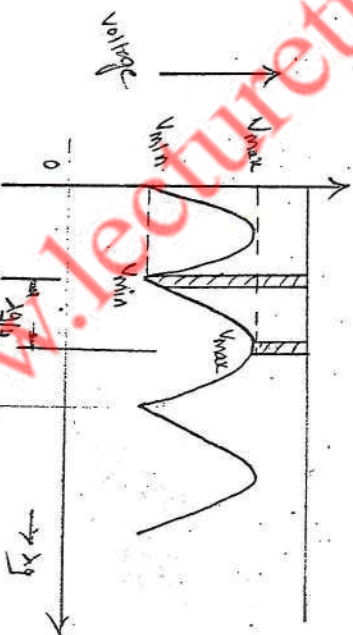


Fig. Setup2, RF substitution method.

Measurement of VSWR :-

Any mismatched load leads to reflected waves resulting in standing waves along the length of the line. The ratio of maximum to minimum voltage gives the VSWR.



$$S = \frac{V_{max}}{V_{min}} = \frac{1+p}{1-p}$$

$$\begin{aligned} \text{if } p=0, S &= 1 \\ p=1, S &= \infty \\ p=0, S &= 1 \end{aligned}$$

Where, ρ = reflection coefficient = $\rho_{\text{reflected}}$

P_{incident}

S varies from 1 to 0

as ρ varies from 0 to 1

Hence minimum value of S is 0 only.

Measurement of Low VSWR's ($S < 10$):

Values of VSWR not exceeding 10 are very easily measured with the set up and can be read off directly on the VSWR meter calibrated as shown in fig.

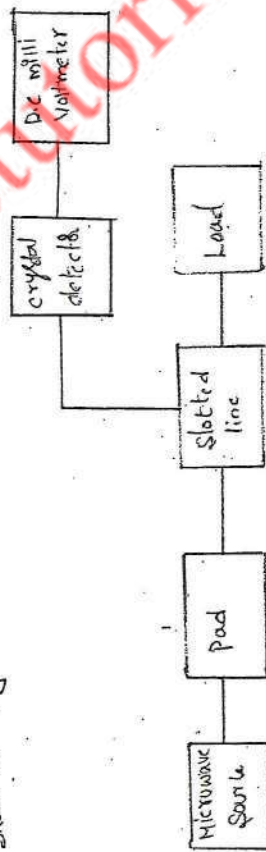


Fig. Microwave test bench for measuring VSWR < 10.

The measurement basically consists of simply adjusting the attenuator to give an adequate reading on the meter, which is a DC millivoltmeter. The probe on the slotted waveguide is moved to get maximum reading on the meter (corresponding to V_{max}). The attenuation is now adjusted to get full scale reading. This full scale reading is noted down. Next the probe on the slotted line is adjusted to get minimum reading on the meter (corresponding to V_{min}). The ratio of first reading to the second (i.e. $V_{\text{max}}/V_{\text{min}}$) gives the VSWR.

The meter itself can be calibrated in terms of VSWR. In case, the probe carriage is moved to give maximum deflection on the VSWR meter by adjusting the pad. This full scale deflection (FSD) corresponds to a VSWR of 1.

for example, for a full scale deflection of 10mV, if the minimum reading on the meter is 1mV then

$$\text{VSWR} = \frac{V_{\text{max}}}{V_{\text{min}}} = \frac{10\text{mV}}{1\text{mV}} = 10$$

If the minimum reading on the meter is 2.5mV then

$$\text{VSWR} = \frac{10\text{mV}}{2.5\text{mV}} = 4$$

If the minimum reading on the meter is 3.3mV then

$$\text{VSWR} = \frac{10\text{mV}}{3.3\text{mV}} = 3$$

If the minimum reading on the meter is 5mV then

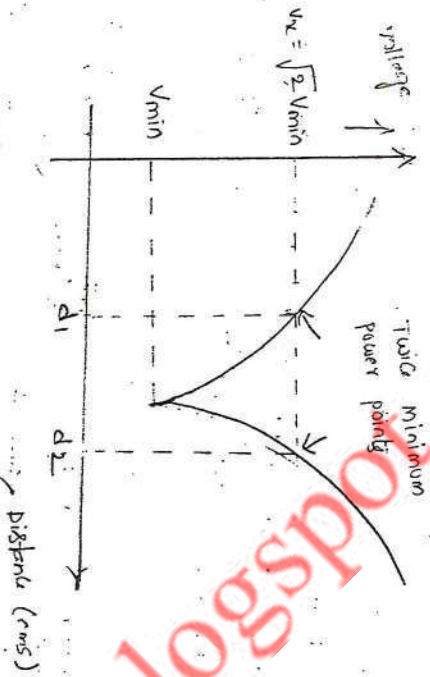
$$\text{VSWR} = \frac{10\text{mV}}{5\text{mV}} = 2$$

When VSWR > 10, the meter will be congested and accurate measurement is not possible. So, the above method is not suitable for VSWR > 10.

High VSWR measurement ($S > 10$):

The method which is used to measure high VSWR i.e. greater than 10 is called as double minimum method. In this method, the probe is inserted to a depth where the minimum can be read without difficulty. The probe is then moved

is a point where the power is twice the minimum. Let this position be noted by d_1 . The probe is then moved to twice the power point on the other side of the minimum (say d_2) as shown in fig. we get $P_{min} \& V_{min}$ → ①



2. $P_{min} \& V_{min}$ → ②

eqn ① $\Rightarrow \frac{1}{2} = \frac{(V_{min})^2}{V_{max}^2}$

eqn ② $V_{max}^2 = 2 (V_{min})^2$

or $V_{max} = \sqrt{2} V_{min}$

Porter for TE_{10} mode, $\lambda_c \approx 2a$

$\lambda_0 = c/f$

$\lambda_g = \frac{\lambda_0}{\sqrt{1 - (\frac{\lambda_0}{\lambda_c})^2}}$

Then V_{SWR} can be calculated using the empirical relation,

$V_{SWR} = \frac{\lambda_g}{\pi(a-d)}$

Measurement of Q of a Cavity Resonator :-

There are several methods for measuring the Q of a Cavity Resonator.

1. Transmission method
2. Impedance measurement
3. Transient decay or decrease method.

Among these, Transmission method is the simplest and is described here in detail.

The set up for Transmission method of measuring Q is shown in fig. In this method, the Cavity Resonator is used as a Transmission device.



Fig. Set up for measurement of Q of a Cavity resonator using Transmission method.

The output signal is measured as a function of the frequency resulting in the resonance curve of shown fig.

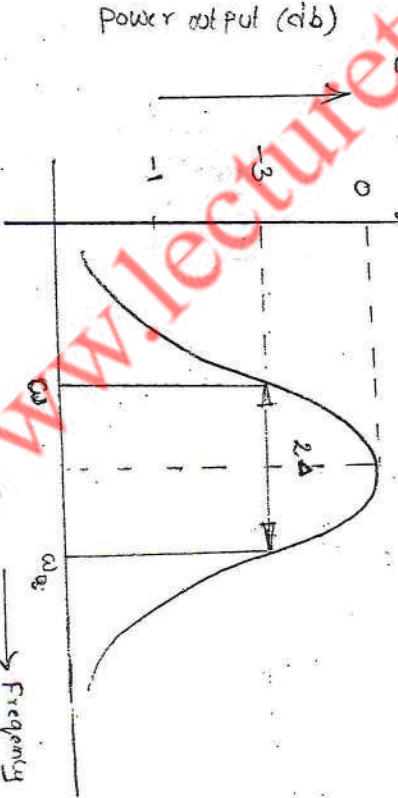


Fig. Resonance Curve

By varying the frequency of microwave source with keeping signal level constant, the output power is measured. Alternately gain can be found by keeping both signal level and frequency constant and output power measured. From the resonance curve half power bandwidth (Δf) can be measured.

(24)

$$\text{i.e. } \Delta f = \pm \frac{1}{Q_L}$$

where Q_L = loaded value,

$$\text{or } Q_L = \pm \frac{1}{\Delta f} = \pm \frac{\omega}{2(\omega - \omega_0)}$$

If the coupling between microwave source and cavity and that between detector and cavity are neglected, $Q_L = Q_0$ (unloaded Q). However, the accuracy of this method is poor, particularly in case of very high Q systems due to narrow band of operation.

Measurement of Impedance:-

Impedance at microwave frequencies can be measured using any of the following 3 methods.

- using magic tee
- using slotted line and
- using network analyzer.

Measurement of Impedance using slotted line:-
Incident and reflected waves will be present proportional to the mismatch of the load under test (whose impedance is to be measured) resulting in standing waves. Using slotted waveguide

and with the load Z_L in the circuit. Given V_{max} and V_{min} can be accurately determined position of V_{max} and V_{min} can be accurately determined.

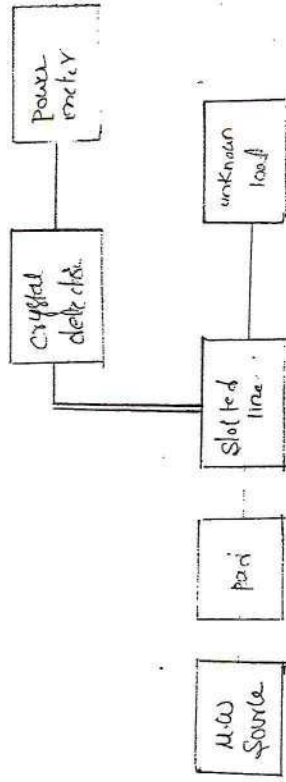


Fig. Setup 1, Impedance measurement using slotted line.

Now the load Z_L is replaced by a short circuit as shown by below. and the shift in minimum is measured. If the minimum is shifted to the left, then the impedance is inductive and it is shift to the right, it is capacitive. unknown impedance can be obtained by usual methods using the data recorded and a Smith chart. Both impedance and reflection coefficient can be obtained in magnitude and phase.



Fig. Setup 2, Impedance measurement using slotted line.

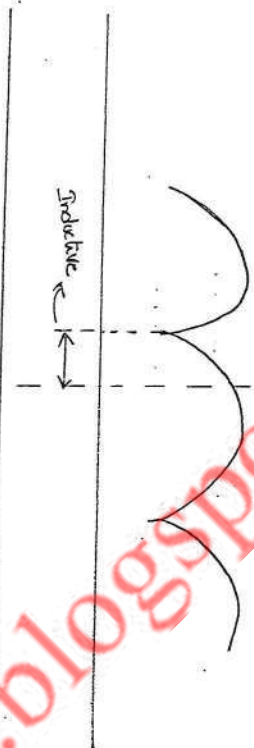
When the load Z_L is replaced by a short circuit and the shift in minimum is measured. If the minimum is shifted to the left, then the impedance is inductive

Setup 1



(25)

Setup 2



Setup 2

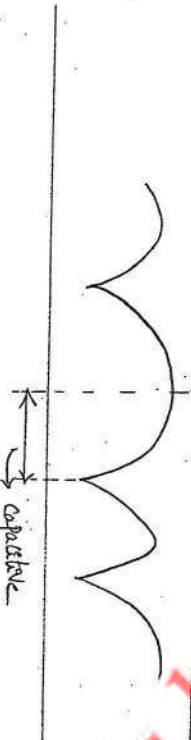


Fig. output standing wave of setup 1 & setup 2.

Measurement of Impedance using Reflectometer:-

The reflectometer indicates magnitude of impedance but not the phase angle, whereas a slotted line overguide measurement gives both. A typical setup for reflectometer technique is shown below where two directional couplers are used to sample the incident power P_i and the reflected power from load. But the directional coupler coefficient k , can be directly obtained in the reflectometer from which impedance can be calculated.

From subdetector reading curve we have,

$$\rho = \sqrt{\frac{P_r}{P_i}}$$

Knowing ρ we can calculate V_{max} and impedance by using the relations,

$$S = \frac{1+\rho}{1-\rho} \text{ and } \frac{Z-Z_0}{Z+Z_0} = \rho.$$

where Z_0 is the wave impedance

Z is unknown impedance.

$$\text{Reflectometer, } \rho = \sqrt{\frac{\text{Reflected power}}{\text{Incident power}}} = \sqrt{\frac{P_r/100}{P_i/100}}$$

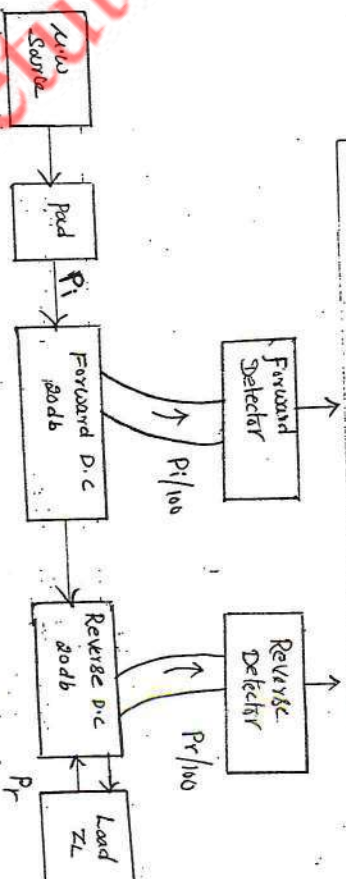


Fig. setup for measuring impedance using reflectometer

Due to directional property of the couplers, there will be no interference between forward and reverse waves. The input power is kept to a low level by means of Pad. The reflection accuracy is greatest at low V_{SWR} (i.e. Subdetector coefficient).

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Calculate the SWR of a Transmission System operating at 10^6 Hz .

Assume TE₁₀ wave T₁₀ inside a waveguide of dimensions

$a = 4 \text{ cm}$, $b = 2.5 \text{ cm}$. The distance measured between two minimum

power points is 1.5 mm on a slotted line.

Given, $f = 10^6 \text{ Hz}$,

$a = 4 \text{ cm}$, $b = 2.5 \text{ cm}$

$$\lambda_0 = \frac{c}{f} = \frac{3 \times 10^{10}}{10 \times 10^9} = 3 \text{ cm}$$

$$d_2 - d_1 = 1.5 \text{ mm}$$

$$\text{We know, } \lambda_g = \frac{\lambda_0}{\sqrt{1 - \left(\frac{a_0}{a}\right)^2}} = \frac{3}{\sqrt{1 - \left(\frac{3/8}{4}\right)^2}} = 3.2 \text{ cm}$$

for double minimum method, VSWR is given by

$$\text{VSWR} = \frac{\lambda_g}{\pi(d_2 - d_1)} = \frac{3.2}{\pi(1.5 \times 10^{-3})} = 10.3$$

two identical directional couplers are used in a waveguide.

To sample the incident and reflected powers, the output of the

couplers is found to be 25 mW and 0.15 mW . Find the value of

VSWR in the waveguide?

Given $P_i = 25 \text{ mW}$

$P_r = 0.15 \text{ mW}$

$$\text{Reflection Coefficient, } \rho = \sqrt{P_r / P_i} = 0.244$$

$$\text{VSWR} = \frac{1 + \rho}{1 - \rho} = \frac{1 + 0.244}{1 - 0.244} = 1.64$$

If we have two directional couplers (as shown) in a

the incident and reflected powers, the output of

couplers are 8 mW and 0.1 mW respectively. what is the value

VSWR in the main waveguide? what is the value of reflected power?

Given $P_i = 8 \text{ mW} \Rightarrow P_r = 0.1 \text{ mW}$

$$\rho = \frac{P_r}{P_i} = \frac{0.1}{8} = 0.125 \Rightarrow P_r = 0.1 \text{ mW}$$

$$\rho = \sqrt{\frac{P_r}{P_i}} = 0.1816$$

$$\text{VSWR (S)} = \frac{1 + \rho}{1 - \rho} = \frac{1 + 0.18}{1 - 0.18} = 1.44$$

two identical series directional couplers are used to sample

incident and reflected power in a waveguide. VSWR = 2 and

the output of the couplers sampling incident power is 45 mW .

what is the value of reflected power?

$$\text{Given, } \text{VSWR} = \frac{1 + \rho}{1 - \rho} = 2$$

$$2 - 2\rho = 1 + \rho \Rightarrow \rho = \frac{1}{3} = 0.33$$

$$\text{We know, } C = 10 \log \frac{P_i}{P_r}$$

$$30 = 10 \log \frac{P_i}{P_r} \Rightarrow \frac{P_i}{P_r} = 10^3$$

$$\rho = \frac{P_r}{P_i} = \frac{P_r}{10^3 P_r} = \frac{1}{10^3}$$

$$\text{Given } \frac{P_i}{1000} = 45 \text{ mW or } P_i = 45 \text{ mW}$$

$$\rho = \sqrt{\frac{P_r}{P_i}} = \sqrt{\frac{P_r}{45 \times 10^{-3}}} \text{ or } \rho = \frac{P_r}{P_i}$$

$$P_r = \rho^2 P_i = 0.510$$

$$C = 20 \text{ dB}$$

$$C = 10 \log \frac{P_i}{P_r}$$

$$20 = 10 \log \frac{P_i}{P_r} \Rightarrow \frac{P_i}{P_r} = 10^2$$

$$\rho = \frac{P_r}{P_i} = \frac{1}{10^2} \rightarrow \text{---}$$

$$C = 10 \log \frac{P_i}{P_r}$$

$$20 = 10 \log \frac{P_i}{P_r} \Rightarrow \frac{P_i}{P_r} = 10^2$$

$$\frac{P_i}{P_r} = 10^2 \Rightarrow \frac{P_r}{P_i} = \frac{1}{10^2} \rightarrow \text{---}$$

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